

## Spectral Gamma-Ray Borehole Log Data Report

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Log Event A

# 50-12-05

**Borehole Information** 

Farm:  $\underline{T}$  Tank:  $\underline{T-112}$  Site Number:  $\underline{299-W10-154}$ 

N-Coord:  $\underline{43,305}$  W-Coord:  $\underline{75,817}$  TOC Elevation:  $\underline{672.00}$ 

Water Level, ft: 98.00 Date Drilled: 1/31/1975

### **Casing Record**

Type: <u>Steel-welded</u> Thickness, in.: <u>0.280</u> ID, in.: <u>6</u>

Top Depth, ft.: 0 Bottom Depth, ft.: 98

Type: Steel-welded Thickness, in. : 0.250 ID, in. : 4

Top Depth, ft. :  $\underline{0}$  Bottom Depth, ft. :  $\underline{98}$ 

Cement Bottom, ft.: 98 Cement Top, ft.: 0

#### **Borehole Notes:**

Borehole 50-12-05 was drilled in December 1974 and January 1975 to a depth of 100 ft. A 6-in. casing was installed from the ground surface to total depth. In July and August 1980, the 6-in. casing was perforated from 0 to 20 ft and 98 to 100 ft and a 4-in. casing was installed inside the 6-in. casing. The annular space between the two casings was filled with grout. The casing thickness is assumed to be 0.237 in. for the 4-in. casing and 0.280 in. for the 6-in. casing.

The tops of both casings are approximately even with the ground surface. The top of casing, which is the zero reference for the SGLS, is at an elevation of 672.0 ft.

## **Equipment Information**

 $\textbf{Calibration Date}: \ \underline{10/1997} \qquad \textbf{Calibration Reference}: \ \underline{GJO\text{-}HAN\text{-}14} \qquad \qquad \textbf{Logging Procedure}: \underline{MAC\text{-}VZCP\ 1.7.10\text{-}1}$ 

## **Logging Information**

Log Run Number: 1 Log Run Date: 12/04/1997 Logging Engineer: Alan Pearson

Start Depth, ft.:  $\underline{0.0}$  Counting Time, sec.:  $\underline{200}$  L/R:  $\underline{L}$  Shield:  $\underline{N}$  Finish Depth, ft.:  $\underline{25.5}$  MSA Interval, ft.:  $\underline{0.5}$  Log Speed, ft/min.:  $\underline{n/a}$ 

Log Run Number: 2 Log Run Date: 12/05/1997 Logging Engineer: Alan Pearson

Start Depth, ft.:  $\underline{24.5}$  Counting Time, sec.:  $\underline{200}$  L/R:  $\underline{L}$  Shield:  $\underline{N}$  Finish Depth, ft.:  $\underline{77.0}$  MSA Interval, ft.:  $\underline{0.5}$  Log Speed, ft/min.:  $\underline{n/a}$ 



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Log Run Number: 3 Log Run Date: 12/08/1997 Logging Engineer: Alan Pearson

Start Depth, ft.: 98.0 Counting Time, sec.: 200 L/R: L Shield: N Finish Depth, ft.: 76.0 MSA Interval, ft.: 0.5 Log Speed, ft/min.: 10/a

#### **Logging Operation Notes:**

The borehole was logged in three runs on December 4, 5, and 8, 1997. The total logging depth achieved by the SGLS was 98.0 ft. Spectra were collected at intervals of 0.5 ft., using a 200-s count time for each interval.

At the time of logging, there was no water in the borehole.

## **Analysis Information**

Analyst: R.G. McCain

Data Processing Reference : MAC-VZCP 1.7.9 Analysis Date : 05/12/1998

### **Analysis Notes:**

The pre-survey and post-survey field verification measurements met acceptance criteria established for peak shape and system efficiency. Energy and resolution calibrations from appropriate verification spectra were used to establish the channel-to-energy conversion and peak resolution parameters used in processing the spectra acquired during the logging operation.

Peak spreading associated with the relatively thick double casing and annular grout was encountered, and many lines associated with naturally occurring radionuclides were poorly defined. Also, the peak recognition software frequently indicated false peaks in the tails of significant peaks, particularly the K-40 peak at 1460.8 keV, the 1764.5-keV peak associated with the U-238 decay chain, and the 2614.6-keV peak associated with the Th-232 decay chain. These peaks were manually deleted.

A casing correction factor for 0.50-in.-thick steel casing was used to determine concentration data over the entire depth. This factor most closely matches the combined thickness of the 4-in. and 6-in. casings.

Concentrations are lower than actual because there is no allowance for the effects of the annular grout between casings.

Shape factor analysis was not performed because there was little indication of man-made radionuclides and because the effects of the dual casing and annular grout on the shape factors are not well understood.

### **Log Plot Notes:**

Separate plots show the man-made and naturally occuring radionuclides. Concentrations are shown as apparent concentrations to reflect the uncertainty associated with the dual casing and annular grout. The headings of the plots identify the specific gamma lines used to calculate concentrations. Uncertainty bars on the plots show statistical uncertainties for the measurements as 95-percent confidence intervals. Open circles on the plot indicate the MDL, which represents the lowest concentration at which positive identification of a gamma-ray peak is statistically defensible.

A combination plot includes man-made and natural radionuclides, the total gamma count rate derived from the



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spectral data, and the Tank Farms gross gamma log. The latest available gamma log is shown on the combination plot. No attempt has been made to adjust the depths of the gross gamma logs to coincide with the SGLS data.

### Results/Interpretations:

The only man-made radionuclide detected in this borehole was Cs-137. Cs-137 contamination was detected intermittently in the upper 20 ft at concentrations near the minimum detectable limit. The maximum value of 0.8 pCi/g was encountered at the ground surface, which can most likely be attributed to migration or carry down of surface contamination.

The KUT concentrations appear to reflect lithological variations with slightly higher concentrations in finer grained material. The SGLS total gamma-ray plot reflects the changes in KUT concentrations detected throughout the logged interval.